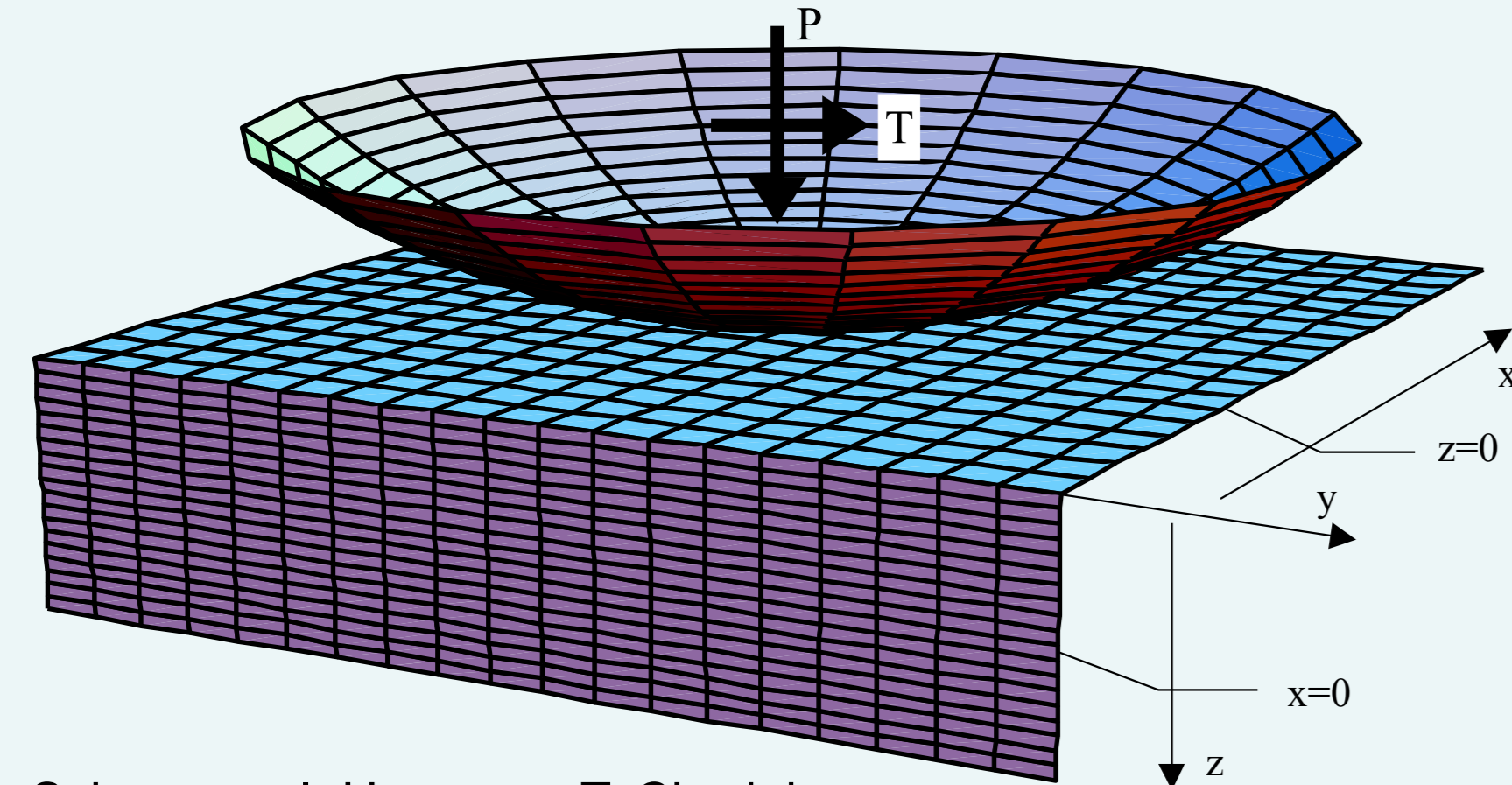
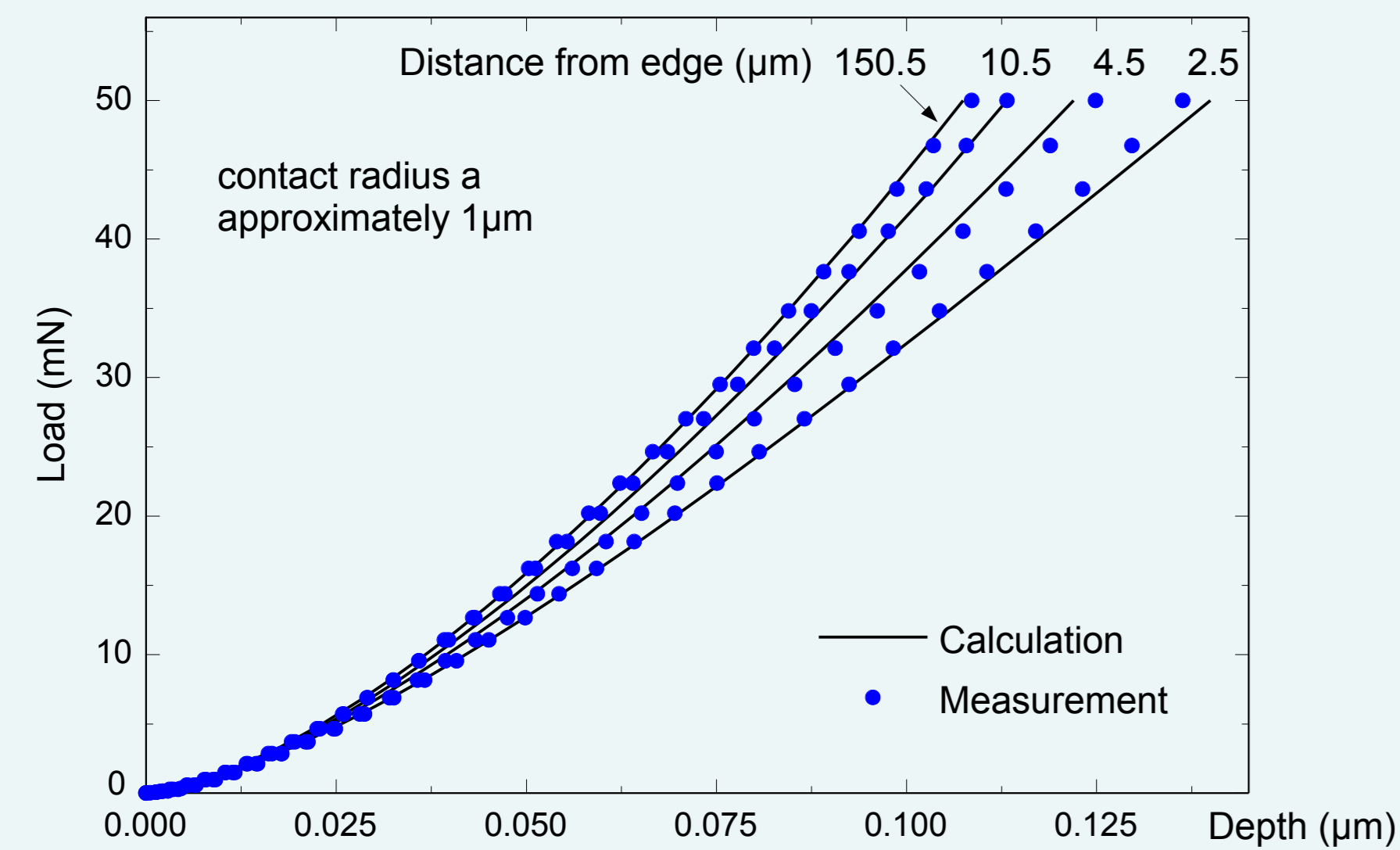


Indentation Measurement Close to an Edge



N. Schwarzer, I. Hermann, T. Chudoba, F. Richter: "Contact Modelling in the Vicinity of an Edge", Surface and Coatings Technology 146-147 (2001) 371-377



Monolithic Case
→ apparently no model problems when $\frac{\text{edge distance}}{a} > 10$

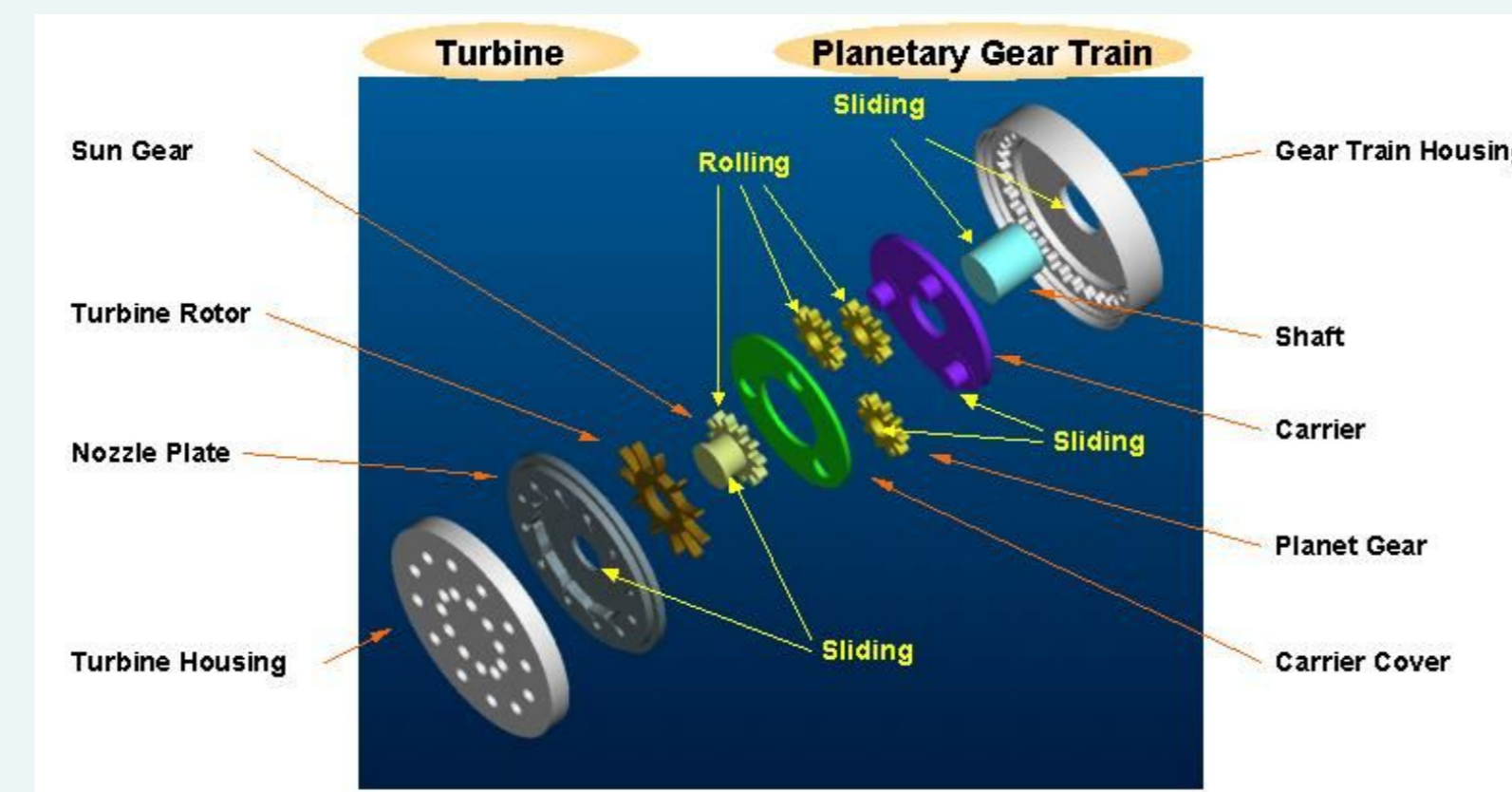
Is this always true? NO!
Yes → normal displacement
No → rest of the elastic field

This is the mathematical basis for proper dimensioning of FE models.

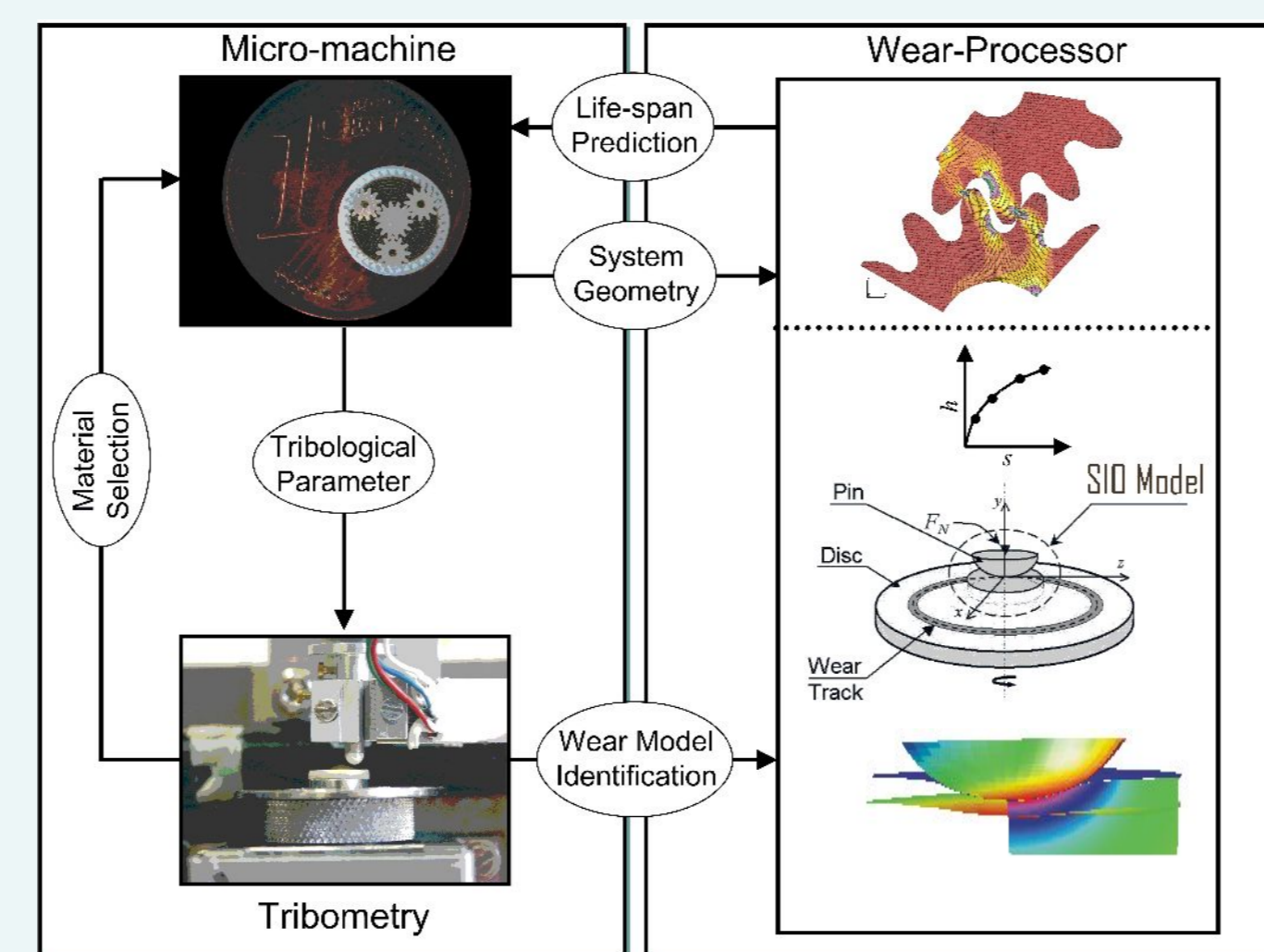
Try for free online at www.siomec.de/services
Find out more: talk E2-3-7 and talk E2-3-9 or SIO-CD in your delegate pack or at booth #14



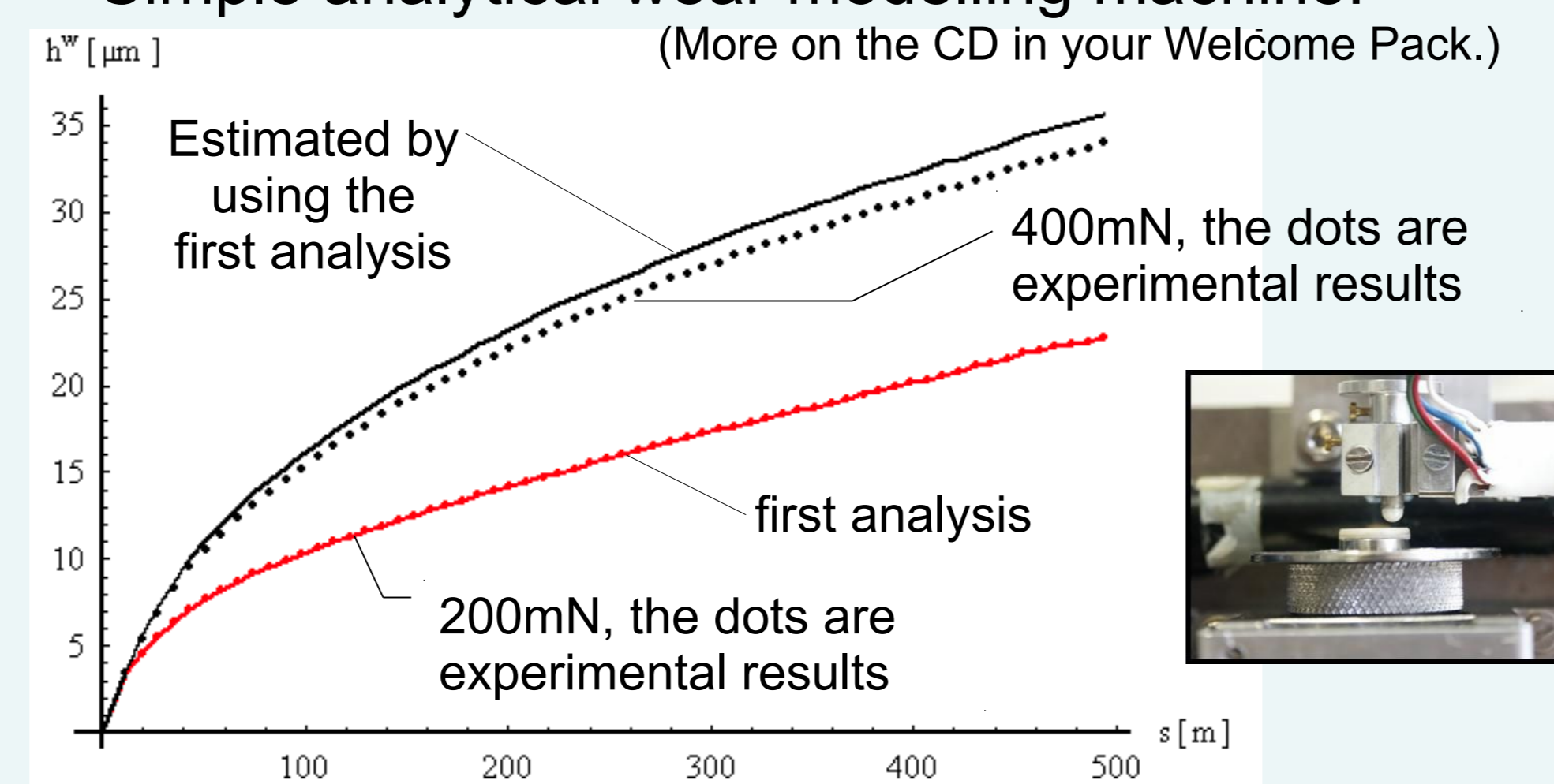
Wear modelling → basis for life time predictions



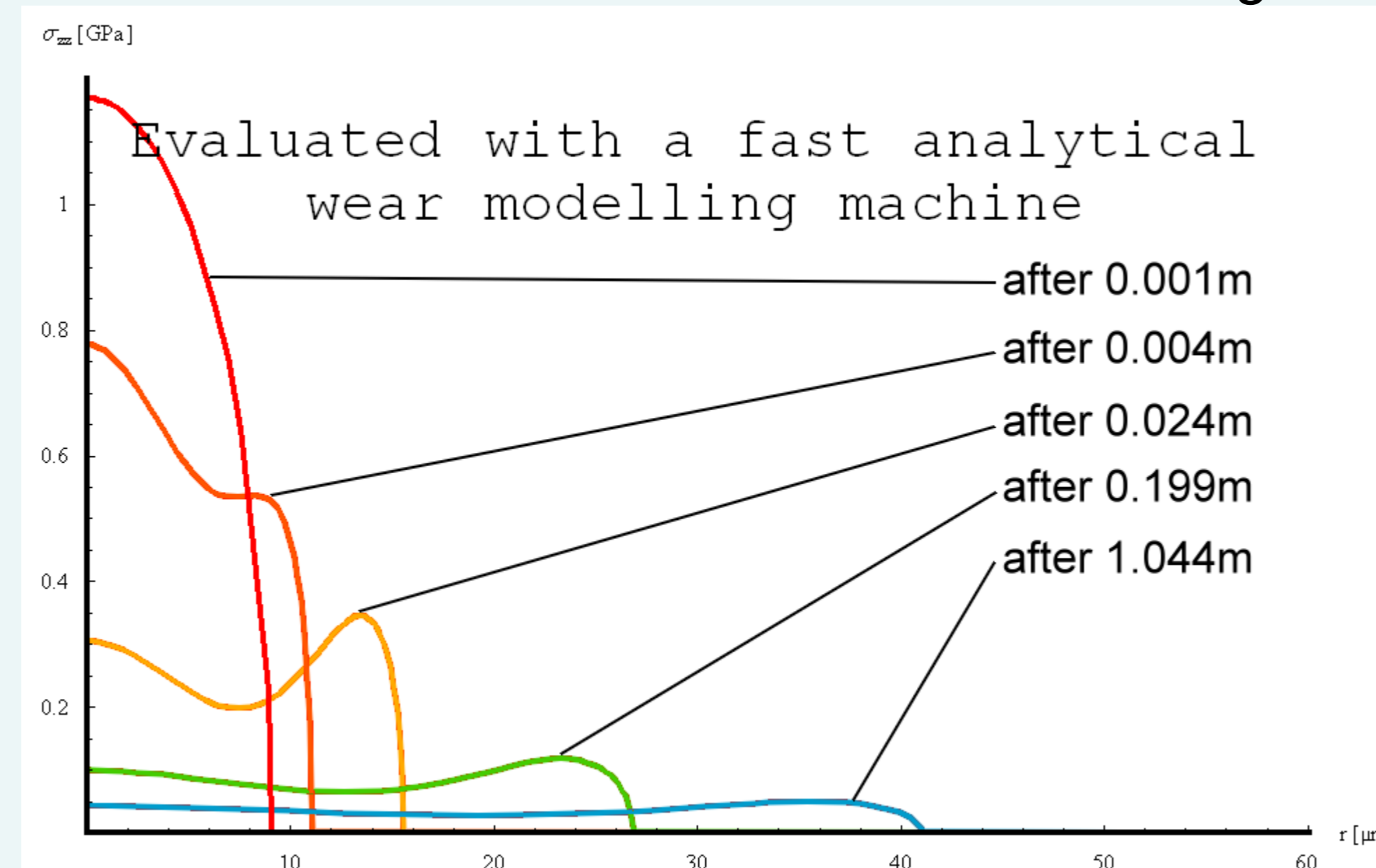
The life time of quite a lot of equipment is mainly limited by wear occurring wherever one finds shearing loads (rolling, sliding, viscous fluids friction etc.)



Simple analytical wear modelling machine: (More on the CD in your Welcome Pack.)



Surface stress as function of wear track length



More details: talk E2-3-7 and try it for free on www.siomec.de/services

Next generation of surface testers

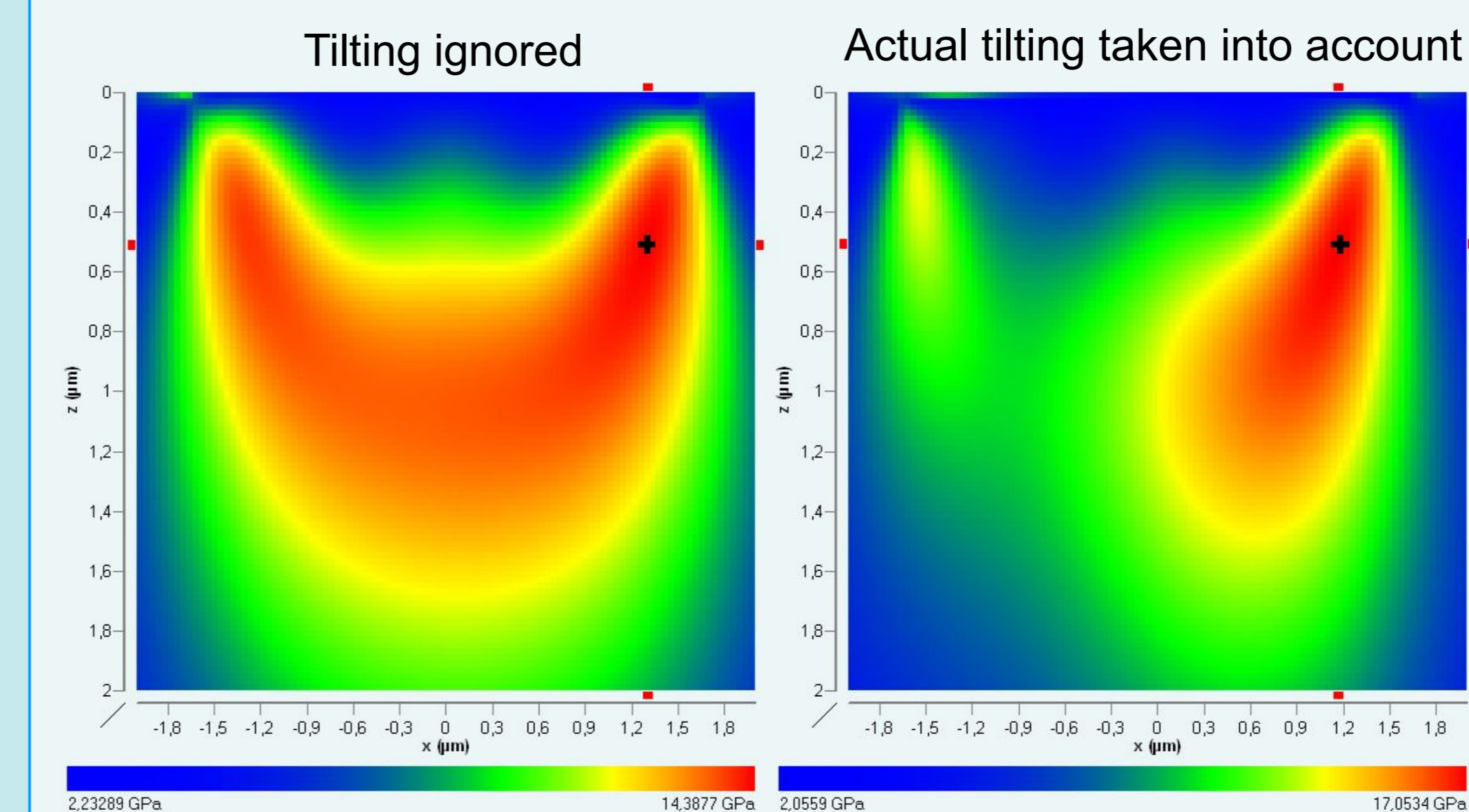
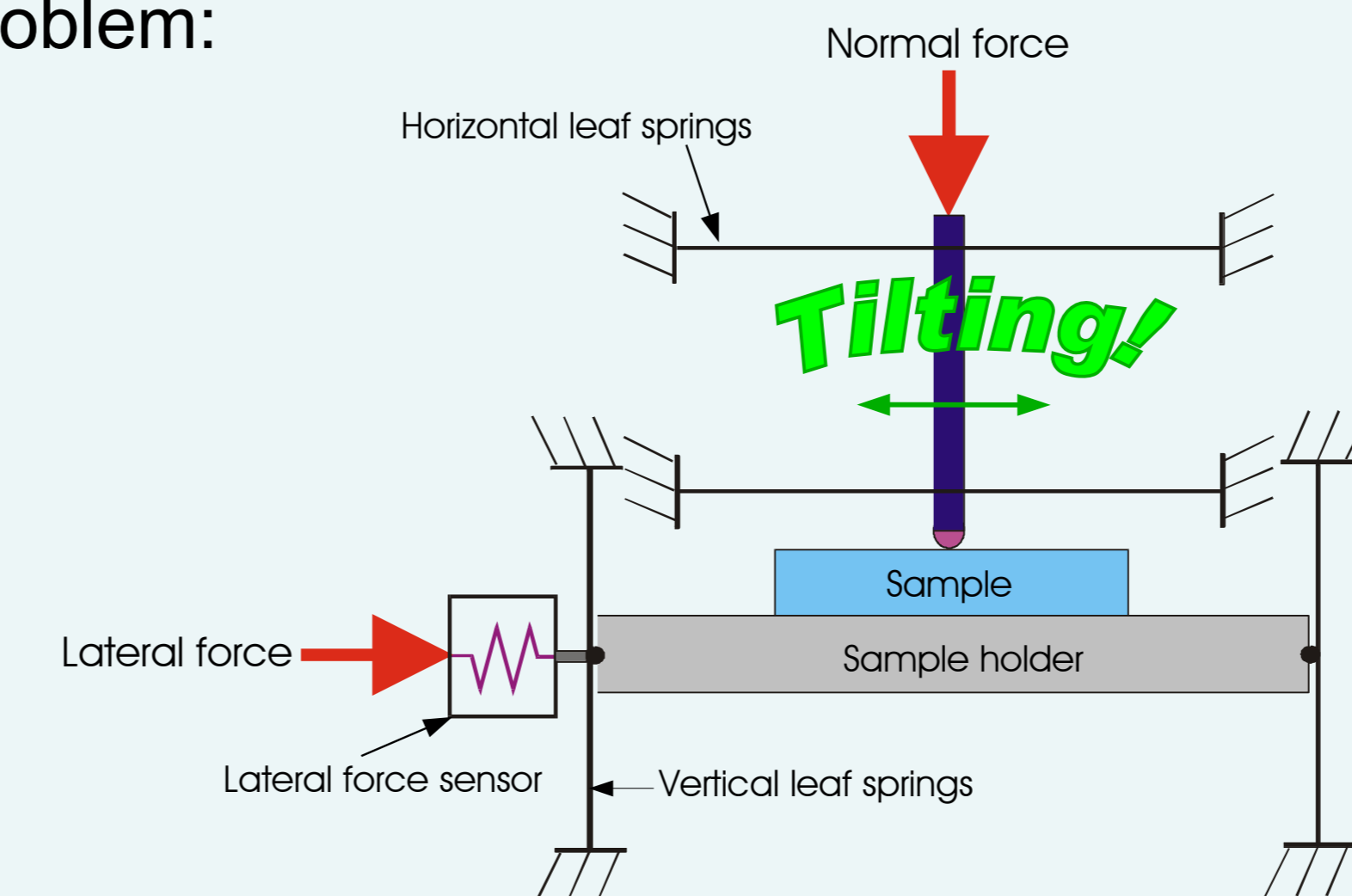
Additional loading components like lateral and rotating loads

→ They allow:

- Intrinsic stress measurement (see CD in your welcome pack or URL below)
- Detection and quantification of anisotropic material properties
- Realistic experimental simulation of practical loading situations



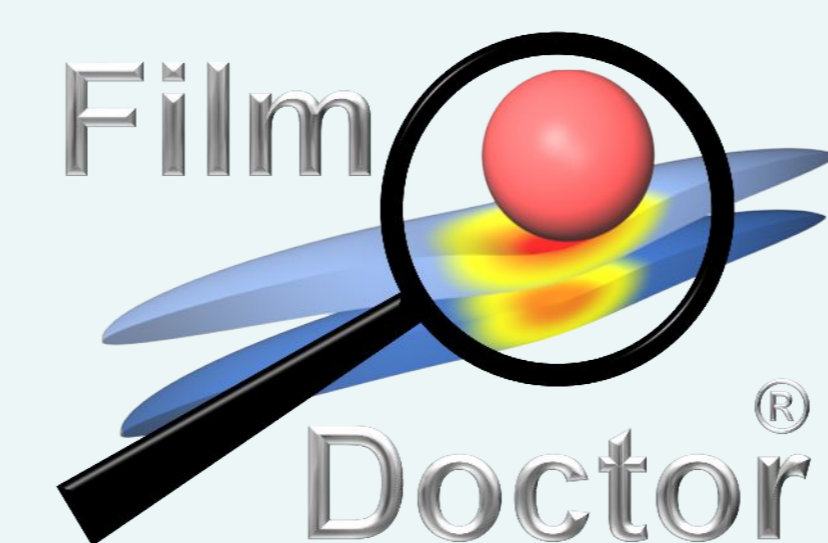
Problem:



Actual tilting angle in an experiment was **only 0.082°**, but caused a completely different stress distribution and an **18% higher maximum of von Mises stress**.

→ The tilting effect should not be ignored!

Evaluation of **complex contact situations** with sliding, rotating, oscillating indenters and taking many side effects like tilting into account will be a breeze if you use our premium software **FilmDoctor®**. It calculates complete stress distributions in a blink due to the used **cutting-edge universal analytical models**.



Try for free (time-unlimited):
• www.siomec.de/FilmDoctor
• CD in your delegate pack

Or watch our presentations:
• booth #14
• talk E2-3-7 and F1-2-8

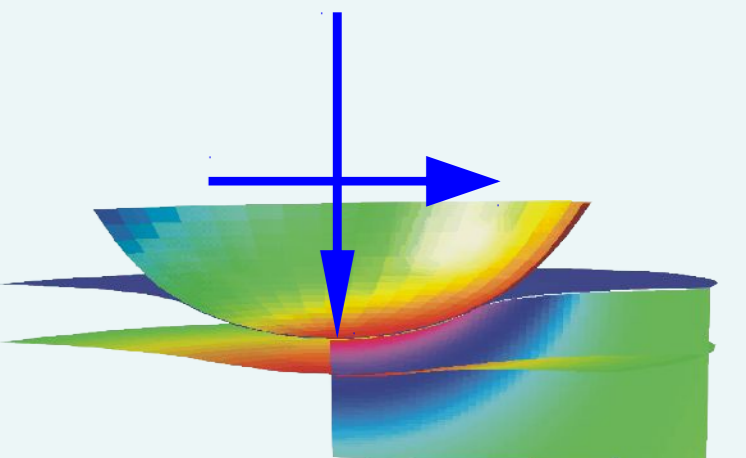


Measuring intrinsic stress with indenter methods

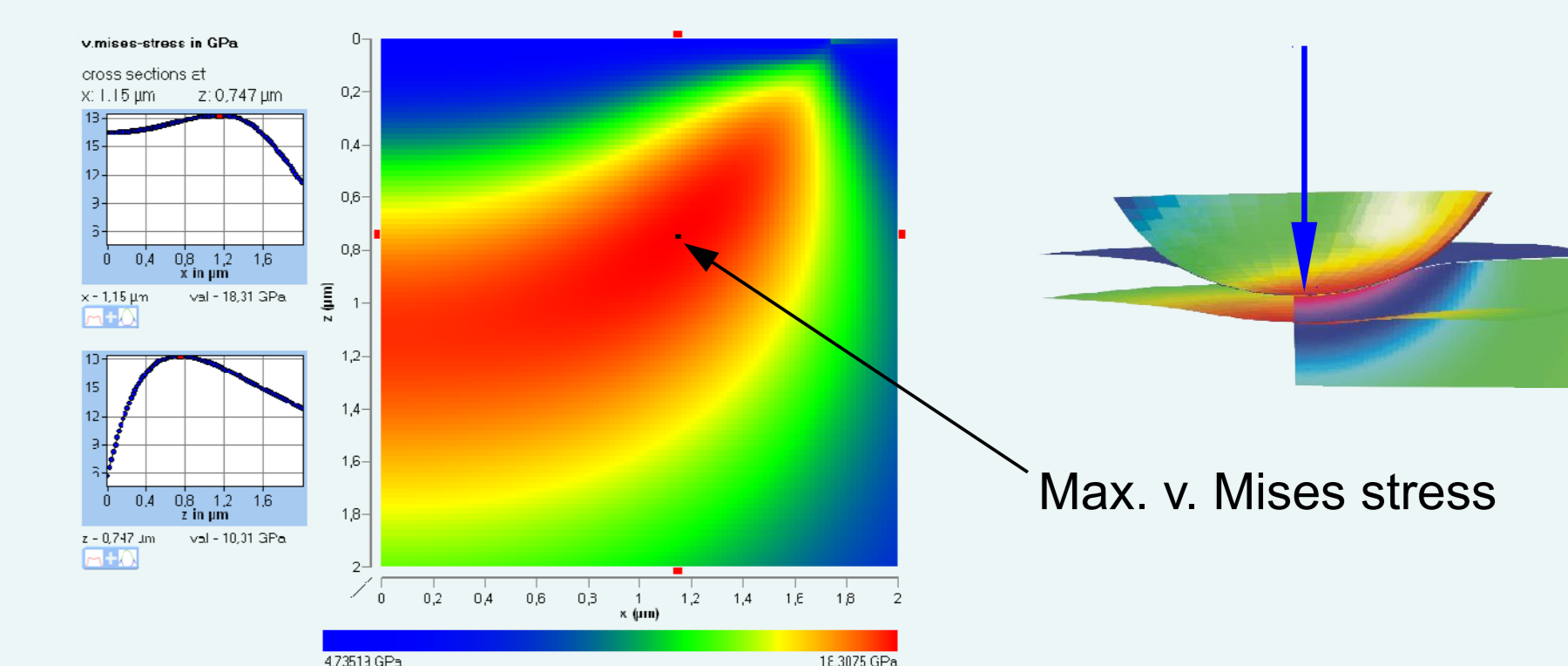
$$\sigma_{rr}^L = \frac{-\sigma_{xx}^L - \sigma_{yy}^L + 2\sigma_{zz}^L \pm \sqrt{4\sigma_M^L - 3((\sigma_{xx}^L - \sigma_{yy}^L)^2 + 3(\tau_{xy}^L^2 + \tau_{xz}^L^2 + \tau_{yz}^L^2))}}{2}$$

Two unknowns require two linear independent measurements:

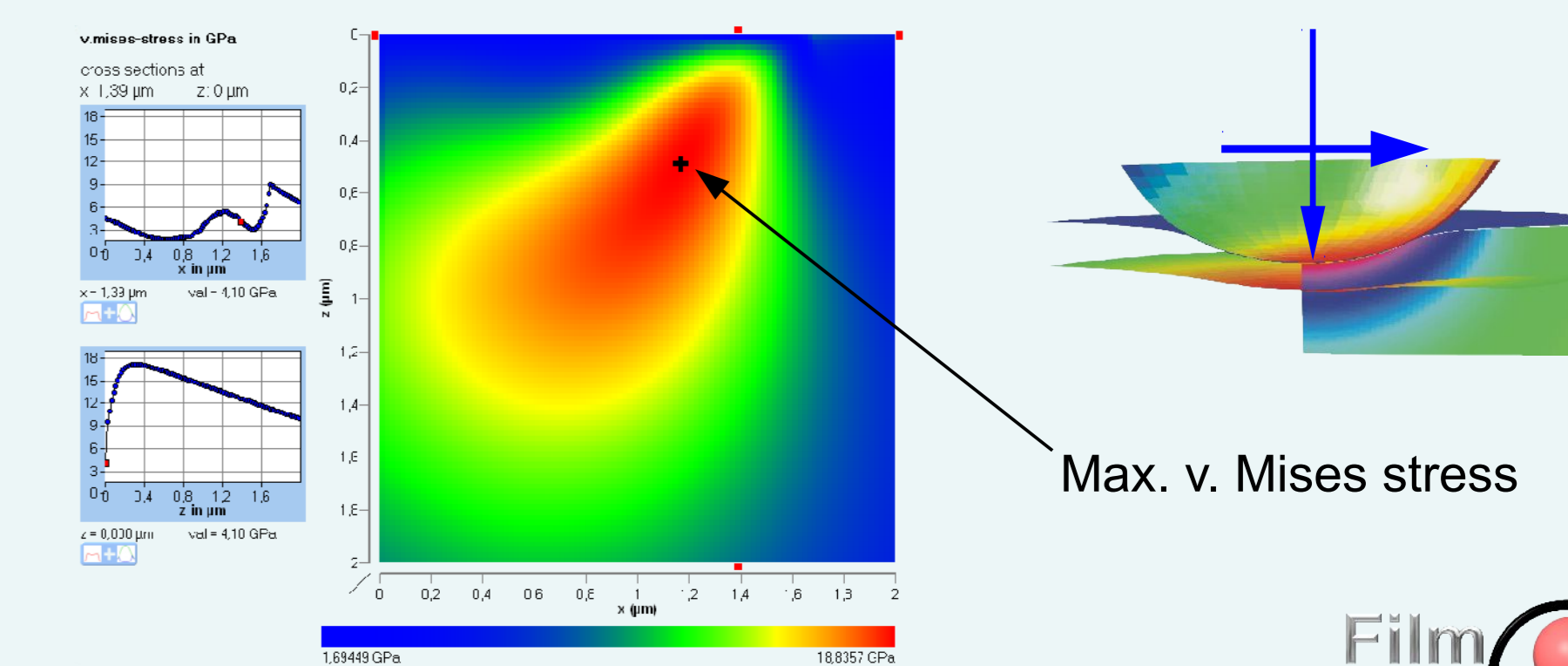
1. Normal Indentation
2. Additional Lateral Load



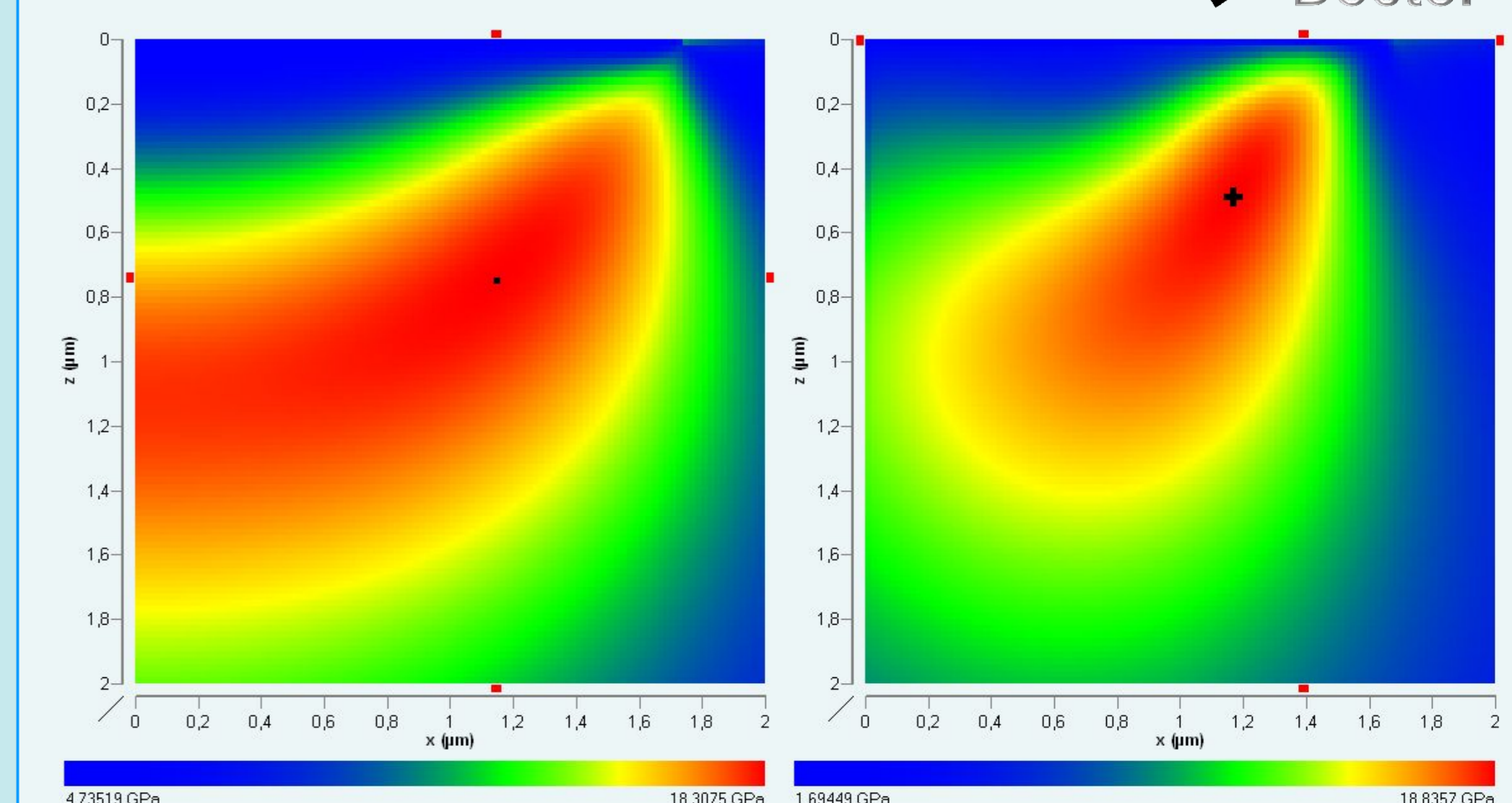
1st step: Normal Indentation



2nd step: Additional Lateral Load



3rd step: Analysis with FilmDoctor®:



Pure yield strength: 16.6GPa
Intrinsic Stress: -2.03GPa

Full story: www.siomec.de/pub/2007/001
Blow by blow account: www.siomec.de/doc/2007/002

Comprehensive Material Database

Yield strength, Critical tensile stress, Young's modulus, Poisson's ratio, thermal expansion coefficient ... of more than 600 materials

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